

Analysis of Reaction Products After Ignition Process of 1-octanol/air Mixtures on a Hot Surface

MARIA MITU^{1*}, ELISABETH BRANDES²

¹Ilie Murgulescu Institute of Physical Chemistry, Romanian Academy, 202 Spl. Independentei, 060021, Bucharest, Romania

²Physikalisch-Technische Bundesanstalt (PTB), Bundesallee 100, 38116 Braunschweig, Germany

1-octanol is considered an alternative to conventional diesel. In order to know the ignition parameters of 1-octanol, an experimental study of the explosive combustion of 1-octanol/air mixtures at ambient pressure and various initial temperatures was performed on a hot stainless-steel surface in a closed vessel. The ignition temperatures of 1-octanol/air mixtures at different initial conditions were determined. Using gas chromatography-mass spectrometry (GC-MS) and gas chromatography with flame ionisation detector (GC-FID) methods, the composition of the reaction products was investigated.

Keywords: ignition, hot stainless-steel rod, 1-octanol, reaction products

Hot surfaces have the potential to ignite explosive gases and vapour/air mixtures. Surfaces may become hot in a number of ways: during the normal operation of plants and processes or as the result of equipment failures (e.g. machinery, parts of combustion engines, electrically heated equipment, including rods and wires, and the hot surfaces and sparks produced by friction between surfaces [1]. With respect to the initiation of explosions, hot surfaces are characterised by the auto ignition temperature defined in standardised methods [2-5].

Ignition due to hot surfaces depends on the initial properties of the flammable gas/air mixture (e.g. composition, concentration, flow pattern, flow velocity) as well as on the material, size and shape of the hot surface [1, 6-14]. In this context, ignition temperatures are particularly useful and have been determined for different combustible mixtures [13,15]. Generally, when the ignition temperatures of combustible mixtures are determined by means of heated wires, rods or cylinders, the temperatures increase with decreasing contact times and heat source dimensions [1, 16-17]. As is well-known, the ability of a flammable mixture to ignite increases significantly with increasing particle temperature [1,18]; however, conditions exist under which an increase in the particle temperature inhibits the ignition of a given mixture. This can happen via reactant depletion in the case of catalytic surfaces [19,21].

The utilisation of hot catalytic surfaces in the combustion of fuels has recently received considerable attention, primarily as a means of reducing pollutant emissions and improving combustion by providing combustion efficiencies. Studies concerning ignition on platinum wires have been reported in [12-14, 20-25].

The need to reduce greenhouse gas emissions and dependence on fossil fuels has driven the search for alternative and renewable fuel sources. Alcohols are regarded as alternative fuels and blending fuel components for internal combustion engines. In the field of diesel engines, alcohols have generated a considerable amount of interest, as their increased oxygenated content can significantly stimulate combustion [26,27]. Many experimental studies about safety characteristics have addressed short-chain alcohols, e.g. [28-31]. Recently, 1-octanol has generated a considerable amount of interest because it can be obtained from biomass. 1-octanol is promising as a new fuel that could be considered an

alternative to conventional diesel [26,27]. To date, very few studies have been carried out concerning the combustion behaviour of 1-octanol. A better understanding requires knowledge of its fundamental combustion characteristics. Studies concerning the combustion of 1-octanol mixtures have been reported in [26,27,32,33].

1-octanol can be considered representative of temperature class T3 [34] substances ($200^{\circ}\text{C} < \text{autoignition temperature} < 300^{\circ}\text{C}$). 1-octanol is manufactured for the synthesis of esters used in perfumes and flavourings. Esters of octanol such as octyl acetate occur as components of essential oils. Octyl acetate is used to evaluate the lipophilicity of pharmaceutical products.

In [1,35,36], a description is given of the fundamental aspects of the initiation of the combustion processes in homogeneous fuel/air mixtures by means of local ignition sources, in addition to a description of the most important notions concerning the explosivity of gaseous mixtures as well as the definitions used in research. Studies concerning the flammability of 1-octanol and other liquid fuel mixtures have been reported in [37-40].

This paper describes the reaction products after ignition of premixed flammable 1-octanol/air mixtures at ambient pressure and different initial temperatures, as well as fuel/air ratios within the explosion limits. The experiments were performed in a closed vessel using a stainless-steel rod as a hot surface. The compositions of the reaction products were investigated using the gas chromatography-mass spectrometry (GC-MS) and the gas chromatography with flame ionisation detector (GC-FID) methods.

Experimental parts

The experimental setup was previously described in detail in [15]. The experimental setup consists of a $2.63 \cdot 10^{-3} \text{ m}^3$ vertical cylindrical explosion vessel, an evaporator tube, a mixing vessel, metering devices for fuel and air, and a heating chamber. The mixture preparation unit designed according to [41] is connected to the explosion vessel. The cylindrical hot surface (stainless-steel rod, surface $2.5 \cdot 10^{-2} \text{ m}^2$, maximum temperature 750°C) equipped with tightly fitting thermocouples is placed in the centre of the explosion vessel. The initial working temperatures were 150 and 175°C . Figure 1 presents the scheme of the experimental equipment.

* email: maria_mitu@icf.ro; Phone: +40-21-3167912

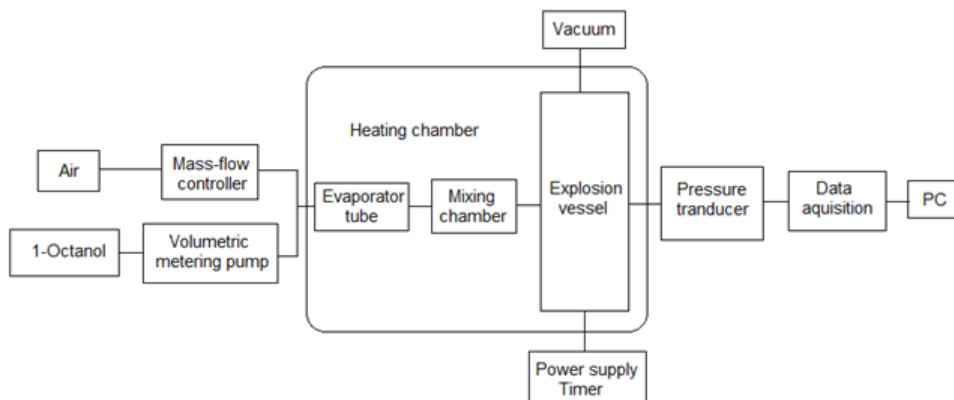


Fig. 1. Scheme of the experimental setup

After ignition takes place, a sample is taken from the end mixture for gas chromatographic analysis using a syringe heated to the starting temperature (150, 175°C). The concentration of n-octanol in the starting vapour/air mixture is varied from 6.0 vol% to 18.0 vol% of n-octanol. Each mixture concentration was investigated at least three times at each temperature.

After each ignition of 1-octanol/air mixtures at ambient pressure and different initial temperatures of these mixtures (150, 175°C), the composition of the combustion products was analysed using gas chromatography-mass spectrometry (GC-MS) and gas chromatography with flame ionisation detector (GC-FID) methods.

Relevant data and safety characteristics of 1-octanol:

- Boiling point, Bp.: 195°C [6];
- Vapor pressure at $T = 20^\circ\text{C}$, p_{22} : 1.3 mbar [42];
- Flash point, Fp: 84°C [6];
- Lower explosion point, LEP: 77.5 °C [38];
- Lower explosive limit at $T_0 = 100^\circ\text{C}$, LEL_{100} : 0.7Vol% [6];
- Upper limit of explosiveness at $T_0 = 150^\circ\text{C}$, UEL_{150} : 6.7 Vol% [6];
- Auto-ignition temperature, AIT: 245°C [6].

Results and discussions

The ignition of flammable gas mixtures on hot surfaces constitutes a hazard in many industries and is a function not only of the type and temperature of the hot surface, but also of the properties of the gas mixture. This study presents results of the ignition process of 1-octanol/air mixtures on a hot stainless-steel rod located in a vertical cylindrical explosion vessel, which differs from ignition on extended surfaces such as heated vessels.

The ignition process occurred at surface temperatures between 330 and 365°C (estimated uncertainty 20°C), which is higher than the auto-ignition temperature (245°C [6]) determined according to a standardised determination method [2-5].

The ignition temperatures of various compositions of the 1-octanol/air mixture were measured at ambient initial pressure and at different initial temperatures of the vapour/air mixtures (150, 175°C). The experimental data at an initial temperature of the 1-octanol/air mixtures of 150°C are given in figure 2 at ambient pressure and different initial compositions. It can be observed that the ignition temperature decreases when the 1-octanol concentration increases.

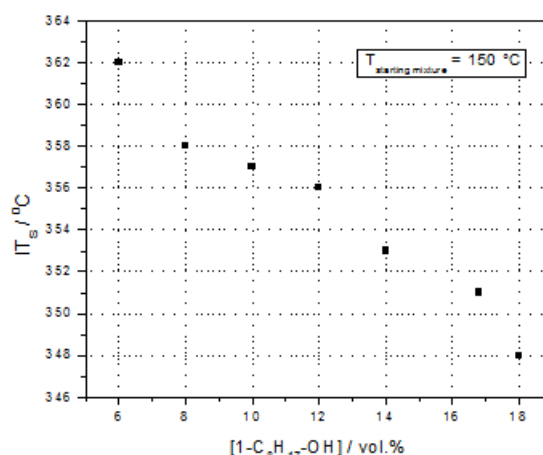


Fig. 2. Ignition temperature of homogenous 1-octanol/air mixtures on a free hot surface (stainless steel) at different initial concentrations and $T_0 = 150^\circ\text{C}$.

Figure 3 and table 1 show the main substances identified in the mixture after ignition: reaction products, N_2 , O_2 and 1-octanol. The identification is based on the NIST database [43]. CO , CO_2 , H_2O and other substances with oxygen atoms in the molecule ($\text{C}_x\text{H}_y\text{O}_z$), saturated hydrocarbons and mostly unsaturated hydrocarbons (alkene, diene, alkyne etc.) were identified.

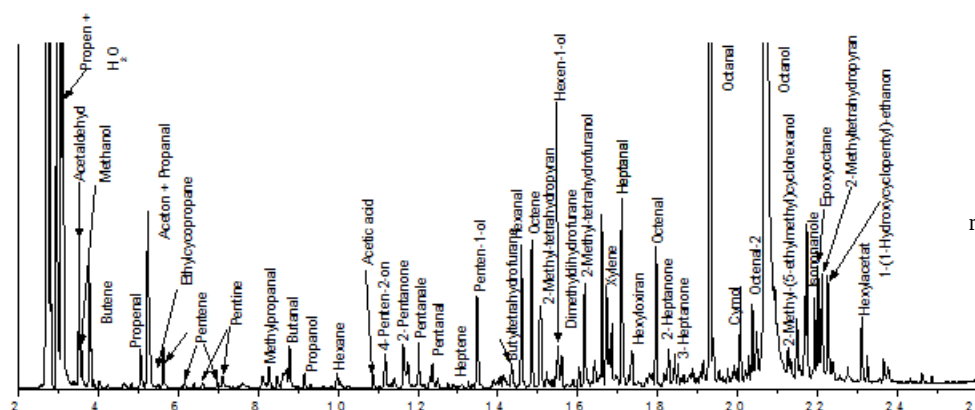


Fig. 3. A typical chromatogram (gas chromatography-mass spectrometry apparatus) of reaction products identified in the mixture after ignition of a 1-octanol/air mixture

Unoxidised reaction products (C_xH_y) in mixture after ignition	
- methane	- pentadiene (isomers)
- ethene	- hexane
- ethyne	- hexene (isomers)
- propene	- hexadiene
- butene (isomers)	- heptene (isomers)
- butadiene	- heptadiene
- pentane	- benzene
- pentene (isomers)	- toluene
- pentene (isomers)	
Oxidised reaction products ($C_xH_yO_z + CO + CO_2$) in mixture after ignition	
- carbon monoxide	- n-pentanal
- carbon dioxide	- n-pentenol
- formaldehyde	- pentanone
- methanol	- propanoic acid
- ethanal	- epoxipentene
- ethoxipropane	- dimethyldihydrofuranone
- acetic acid	- hexanone
- propenol	- tetrahydromethylpyranone
- propanol	- heptanone (isomers)
- propenal	- butyltetrahydrofuran
- propanal	- hexanal
- acetone	- heptanal
- epoxibutane	- octene
- 2-butenone	- octadiene
- 2-butanone	- octanal
- butanal	- nonanol
- butenole	- butylcyclopentanol
- methylfuran	- water
- tetrahydrofuran	

Table 1
MAIN REACTION PRODUCTS IDENTIFIED IN THE MIXTURES AFTER IGNITION

In all experiments, the same reaction products were found (albeit in different proportions). This is also valid for previous experiments carried out with 1-octanol at ambient pressure during the determination of the auto-ignition temperature according to EN 14522 [2] or at higher pressures (determination of autoignition temperature in a 0.5 l autoclave); thus, the conclusion can be drawn that the basic reaction mechanism of the oxidation reactions [44] did not change.

Compared to the reaction product of n-Heptane /air mixtures that had comparable compositions and starting temperatures [15], more oxidised species, especially short-chain alcohols, were detected in the burnt 1-octanol/air mixtures as expected, whereas more cyclic and unsaturated compounds were detected with n-Heptane/air mixtures.

In order to simplify the quantification, all reaction products containing oxygen were grouped as oxidised reaction products, while the hydrocarbons were grouped as unoxidised reaction products (C_xH_y). CO and C_2H_4 were chosen to represent the short-chain reaction products. The relative uncertainty of the quantification of the reaction products in the end mixtures is estimated to be 20%.

For each experimental test, all reaction products identified were present in every burnt end mixture

independent of the 1-octanol concentration and the starting temperature.

Figure 4 shows the variation of the relative amount of O_2 consumed and the relative amount of 1-octanol consumed.

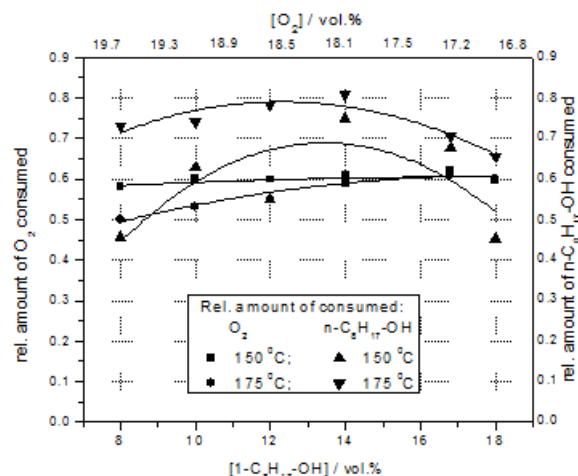


Fig. 4. Relative amount of O_2 consumed and of 1-octanol consumed, compared to the respective composition of the starting 1-octanol/air mixtures.

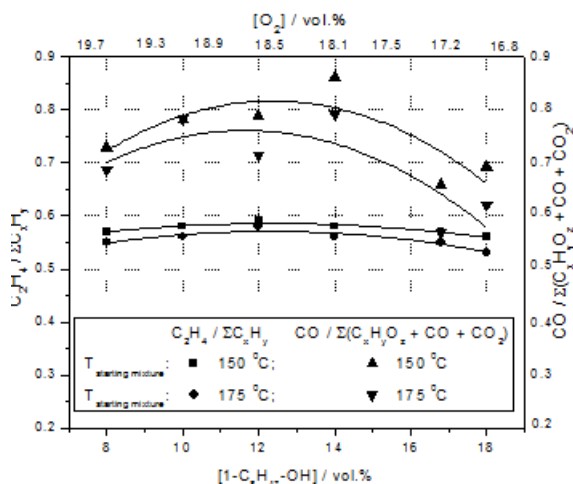


Fig. 5. Ratio of $C_2H_4 / \Sigma C_{x_y}H_y$ and of $CO / \Sigma(C_{x_y}H_{y_z}O_z + CO + CO_2)$ compared to the respective composition of the starting 1-octanol/air mixtures

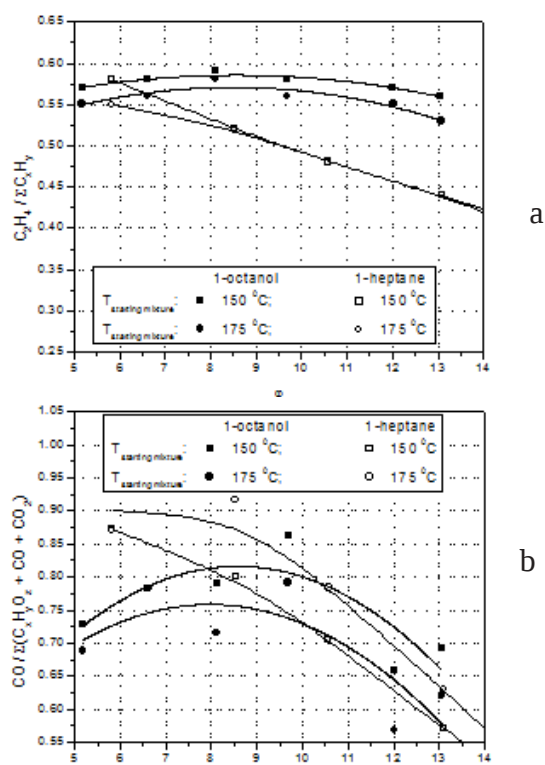


Fig. 6. Ratio of $C_2H_4 / \Sigma C_{x_y}H_y$ of $CO / \Sigma(C_{x_y}H_{y_z}O_z + CO + CO_2)$ compared to the stoichiometric concentration of the starting 1-octanol/air mixtures and 1-heptane/air mixtures at different initial temperatures

The plots indicate that there is no real influence of the temperature on the ratios of $C_2H_4 / \Sigma C_{x_y}H_y$ within the temperature range investigated, whereas the ratio of $CO / \Sigma(C_{x_y}H_{y_z}O_z + CO + CO_2)$ shows a clear maximum (fig. 5).

Comparing these ratios - $C_2H_4 / \Sigma C_{x_y}H_y$ and $CO / \Sigma(C_{x_y}H_{y_z}O_z + CO + CO_2)$ - with the respective ratios of 1-heptane/air mixtures of the same equivalence ratio ϕ [15] (the equivalence ratio ϕ of any flammable mixture is defined

as: $\phi = \frac{[fuel]/[oxygen]}{[fuel]_{st}/[oxygen]_{st}}$, where the index *st* refers to the

stoichiometric concentration of the fuel-air mixture), the following statements can be made:

-Although starting at similar $C_2H_4 / \Sigma C_{x_y}H_y$ ratios, this ratio decreases with increasing 1-heptane concentration,

whereas this ratio is more or less independent with 1-octanol (fig. 6a).

-Although the maximum ratio of $CO / \Sigma(C_{x_y}H_{y_z}O_z + CO + CO_2)$ (about 0.9) is comparable in both cases, the maximum appears at different starting compositions and the decrease is more distinct with 1-heptane mixtures.

Conclusions

This study investigated the reaction products of 1-octanol/air mixtures after ignition by a cylindrical hot surface (stainless-steel rod) in a cylindrical closed vessel at ambient pressure and different initial temperatures, as well as fuel/air ratios within the explosion limits. The ignition temperatures for various 1-octanol/air mixtures (6 vol% – 18 vol%) at 150°C were reported.

Using the gas chromatography-mass spectrometry (GC-MS) and the gas chromatography with flame ionisation detector (GC-FID) methods, the composition of the reaction products was investigated. In all the ignition-process experiments, the same reaction products were found in different proportions.

It has been observed that the amount of the 1-octanol and oxygen that undergoes the reactions is only slightly dependent on the initial starting temperature of the vapour/air mixture over the whole concentration range. From the ratios of $CO / \Sigma C_{x_y}H_{y_z}O_z$ and $C_2H_4 / \Sigma C_{x_y}H_y$, it has been observed that, by increasing the 1-octanol content in the starting mixture, the amount of the short-chain reaction products is reduced for the benefit of reaction products with a chain length of C_3 and higher. As expected, the number of oxidated reaction products is higher when compared to n-heptane/air mixtures.

References

1. STEEN, H., GOEDDE, M., BOTHE, H., Handbook of Explosion Prevention and Protection. Ed. HATTWIG, M., STEEN, H., Wiley-VCH, Ignition by hot surfaces, 2004, Chap. 2.3.
- 2.*** DIN EN 14522, Determination of the auto ignition temperature of gases and vapours, Beuth Verlag, Berlin, 2005.
- 3.*** IEC 60079-4, Electrical apparatus for explosive gas atmospheres. Part 4: Method of test for ignition temperature, IEC, Geneva, Switzerland, 1975.
- 4.*** DIN 51794, Prüfung von Mineralalkohlenwasserstoffen - Bestimmung der Zündtemperatur, Beuth Verlag, Berlin, 2003.
- 5.*** ASTM E659-78, Standard Test Method for Autoignition Temperature of Liquid Chemicals, ASTM International, West Conshohocken, PA, USA, 2005.
- 6.*** CHEMSAFE® Database for Recommended Safety Characteristics, BAM, PTB, DECHEMA, Germany, 2014.
7. GOODALL, D.G., INGLE, R., Fire resistance of industrial fluids, The ignition of flammable fluids by hot surfaces, American Society for Testing and Materials, 1966, p. 64.
8. BOTHE, H., STEEN, H., The ignition of flammable vapours by hot pipes and plots, 6th Int. Sym. Loss Prev. Safety Prom. **3** no. 85, 1989, p. 1.
9. GOSDA, G., OELMEYER, R., SCHACKE, H., WALTHER, C.-D., Hot pipelines-Ignition Source or not?, 6th Int. Sym. Loss Prev. Safety Prom. **3** no. 13, 1989, p. 1.
10. UENGUET, H., CFD simulation and detailed chemical modelling of alkane autoignition near heated metal surface; Shell Global Solutions, Research report 352, 2001.
11. MULLEN, J.W., FENN, J.B., IRBY, M.R., The ignition of high velocity streams of combustible gases by heated cylindrical rods, 3rd Symp. Comb. Flame, Baltimore, 1949, p. 317.
12. OANCEA, D., RAZUS, D., MITU, M., CONSTANTINESCU, S., Hot wire ignition of premixed flammable fuel-air mixtures using isothermally heated platinum wires, Rev. Roum. Chim., **47**, no. 1-2, 2002, p. 91.

- 13.OANCEA, D., RAZUS, D., MITU, M., Critical temperature-pressure data for ignition of stagnant propylene-air mixtures on platinum filaments, *Rev. Roum. Chim.*, **50**, no. 11-12, 2005, p. 991.
- 14.MUNTEANU, V., MITU, M., OANCEA, D., Incipient phase of the catalytic ignition of lean n-heptane-air mixture, *Anal. Univ. Bucuresti -Chimie* **19**, no. 1, 2010, p. 49.
- 15.MITU, M., BRANDES, E., Investigation of reaction products obtained from ignition process of n-heptane / air mixtures on free hot surface, *Rev. Chim. (Bucharest)*, **68**, no. 5, 2017, p. 1035.
- 16.LEWIS, B., von ELBE, G., *Combustion, Flames and Explosions of Gases*, Second Ed., Academic Press Inc., New York and London, 1961.
- 17.BOECK, L.R., MEIJERS, M., KINK, A., MEVEL, R. SHEPHERD, J.E., Ignition of fuel-air mixtures from a hot circular cylinder, *Combust. Flame*, **185**, 2017, p. 265.
- 18.LAURENDEAU, N.M., Thermal ignition of methane-air mixtures by hot surfaces: a critical examination, *Combust. Flame*, **46**, 1982, p.29.
- 19.LAW, C.K., CHUNG, S.H., Thermal and catalytic inhibition of ignition through reactant depletion, *Combust. Sci. Technol.*, **32**, 1983, p. 307.
- 20.GRIFFIN, T.A., PFEFFERLE, L.D., Gas phase and catalytic ignition of methane and ethane in air over platinum, *AIChE J.*, **36**, no. 6, 1990, p. 861.
- 21.OANCEA, D., MITU, M., PINCU, E., RAZUS, D., Temperature inhibiting effect on the ignition of a lean propylene-air mixture by an isothermally heated platinum filament, *Rev. Roum. Chim.* **49**, no. 3-4, 2004, p. 391.
- 22.OANCEA, D., MUNTEANU, V., RAZUS, D., MITU, M., A simplified kinetic model for isothermal catalytic ignition propane/air mixture on platinum wire, *J. Therm. Anal. Calorim.*, **103**, no. 3, 2011, p. 911.
- 23.MITU, M., RAZUS, D., OANCEA, D., Coupled catalytic-gas phase ignition of propane-oxygen-inert mixtures on an isothermally heated platinum filament supported on a bar quartz, *Rev. Chim. (Bucharest)*, **69**, no. 4, 2018, p. 870
- 24.PFEFFERLE, L.D., GRIFFIN, T.A., WINTER, M., CROSLEY, D.R., DYER, M.J., The influence of catalytic activity on the ignition of boundary layer flows. Part I: Hydroxyl radical measurements, *Comb. Flame*, **76**, 1989, p. 325.
- 25.PFEFFERLE, L.D., GRIFFIN, T.A., WINTER, M., CROSLEY, D.R., DYER, M.J., The influence of catalytic activity on the ignition of boundary layer flows. Part II: Oxygen atom measurements, *Comb. Flame*, **76**, 1989, p. 339.
- 26.KERSCHGENS, B., CAI, L., PITSCH, H., HEUSER, B., PISCHINGER, S., Di-n-buthylether, n-octanol, and n-octane as fuel candidates for diesel engine combustion, *Combust. Flame*, **163**, 2016, p. 66.
- 27.RAJESH KUMAR, B., SARAVANAN, S., RANA, D., ANISH, V., NAGENDRAN, A., Effect of a sustainable biofuel - n-octanol - on the combustion, performance and emissions of a DI diesel engine under naturally aspirated and exhaust gas recirculation (EGR) modes, *Energy Convers. Manage.*, **118**, 2016, p. 275.
- 28.MITU, M., BRANDES, E., Explosion parameters of methanol-air mixtures, *Fuel*, **158**, 2015, p. 217.
- 29.BRANDES, E., FROESE, D.H., MITU, M., Safety characteristics of ethanol / automotive petrol mixtures, *Oil Gas European Magazine* **4**, 2006, p. 199.
- 30.MITU, M., BRANDES, E., Sicherheitstechnische Kenngrößen von Alkohol/Luft-Gemischen - Explosionsdruck, zeitlicher Druckanstieg, Verbrennungsgeschwindigkeit, *Proc. 13. BAM-PTB-Kolloquium zur chemischen und physikalischen Sicherheitstechnik*, Braunschweig, Germany, 2013.
- 31.MITU, M., BRANDES, E., Influence of pressure, temperature and vessel volume on explosion characteristics of ethanol/air mixtures in closed spherical vessels, *Fuel*, **203**, 2017, p. 460.
- 32.BHARTI, A., BANERJEE, T., Reactive force field simulation studies on the combustion behavior of n-octanol, *Fuel Processing Technol.*, **152**, 2016, p. 132.
- 33.CAI, L., UYGUN, Y., TOGBE, C., PITSCH, H., OLIVIER, H., DAGAUT, P., SARANTHY, S.M., An experimental and modeling study of n-octanol combustion, *Proc. Combust. Inst.*, **35**, 2015, p. 419.
- 34.***DIN EN 60079-0, Elektrische Betriebsmittel für gasexplosionsge fardete Bereiche -Teil 0: Allgemeine Anforderungen, Beuth Verlag, Berlin, 2004.
- 35.RAZUS, D., OANCEA, D., IONESCU, N.I., Initierarea exploziilor in amestecuri gazease omogene combustibil-oxidant. I. Initierarea exploziilor cu ajutorul corpurilor incalzite, *Rev. Chim.(Bucharest)*, **51**, no. 8, 2000, p. 590.
- 36.RAZUS, D., OANCEA, D., IONESCU, N.I., GOSA, V., Explozivitatea amestecurilor gazease omogene. Parametri caracteristici, *Rev. Chim.(Bucharest)*, **45**, no. 12, 1994, p. 1097.
- 37.BRANDES, E., MITU, M., PAWEL, D., Flash point or lower explosion point-which one to choose for explosion prevention, *Proceedings of European Combustion Meeting*, Belgium, 2005.
- 38.MITU, M., BRANDES, E., PAWEL, D., Lower explosion limits, lower explosion points and flash points of (1-octanol + n-amyl acetate) mixtures, *Rev. Chim. (Bucharest)*, **57**, no. 7, 2006, p. 770.
- 39.BRANDES, E., MITU, M., PAWEL, D., The Lower Explosion Point - a Good Measure for Explosion Prevention: Experiment and calculation for pure compounds and some mixtures, *J. Loss Prev. Proc. Ind.* **20**, 2007, p. 536.
- 40.BRANDES, E., ECKERT, K., HERRMANN, P., MITU, M., Vapour pressures can be calculated for regulatory purposes, *European Coatings Journal*, **10**, 2008, p. 34.
- 41.*** DIN EN 1839, Determination of explosion limits of gases and vapours, Beuth Verlag, Berlin, 2004.
- 42.WEST, R.C., *Handbook of Chemistry and Physics, A Ready-Reference Book of Chemical and Physical Data*, 50th Edition 1970-1971, The Chemical Rubber Co. 18901 Cranwood Parkway, Cleveland, OH, 44128 USA, p. D-146.
- 43.*** NIST, Mass Spectral Database, 2000.
- 44.GOEDDE, M., BRANDES, E., CAMMENG, H. K., Zündtemperatur homologer Reihen. Teil 1: Untersuchungen bei Normaldruck, *PTB-Mitteilungen*, 108 no. 2, 1998, p. 80.

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